## Optimal Control of the Thermistor Problem

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The presented talk deals with the optimal control of the thermistor problem that models the conductive heat transfer in a conductor produced by an electric current. This leads to the following quasi-linear system of partial differential equations (PDEs):

$$\partial_t \theta - \operatorname{div}(\kappa \nabla \theta) = (\sigma(\theta) \nabla \varphi) \cdot \nabla \varphi \quad \text{in Q}$$
(1)

$$\nu \cdot \kappa \nabla \theta + \alpha \theta = \alpha \theta_l \quad \text{on} \Sigma \tag{2}$$

$$\theta(0) = \theta_0 \quad \text{in } \Omega \tag{3}$$

$$-\operatorname{div}(\sigma(\theta)\nabla\varphi) = 0 \quad \text{in } Q \tag{4}$$

$$\nu \cdot \sigma(\theta) \nabla \varphi = u \quad \text{on } \Sigma_0 \tag{5}$$

$$\varphi = 0 \quad \text{on } \Sigma \backslash \Sigma_0, \tag{6}$$

with a Lipschitz domain  $\Omega \subset \mathbf{R}^2$ ,  $Q = \Omega \times ]0, T[, \Sigma = \partial\Omega \times ]0, T[$ , and  $\Sigma_0 = \Gamma_0 \times ]0, T[$ , where  $\Gamma_0$  denotes a fixed part of  $\partial\Omega$ . Moreover,  $\theta$  represents the temperature, while  $\varphi$  is the electric potential. Furthermore,  $\theta_l$  and  $\theta_0$  are given functions, and u is the control that can be interpreted as a current induced on  $\Gamma_0$ . A possible application for this coupled system of PDEs is the hardening of steel workpieces via the Joule effect.

Our aim is to adjust the control u such that

$$J(\theta, u) := \frac{1}{2} \|\theta(T) - \theta_d\|_{L^2(\Omega_m)}^2 + \frac{\beta}{2} \|u\|_{L^2(\Sigma_0)}^2$$
(7)

is minimized subject to (1)-(6) and the following inequality constraints

$$u_a \le u(t, x) \le u_b$$
 a.e. on  $\Sigma_0$  (8)

$$\theta_a(t,x) \le \theta(t,x) \le \theta_b(t,x) \quad \text{a.e. in } Q.$$
(9)

Here, (8) reflects the maximum available electrical power, whereas (9) prevents melting of the material which is crucial in view of hardening applications. Notice that (9) represents a pointwise state constraint that is known to be numerically and theoretically challenging to handle. To be more precise, the generalized Karush-Kuhn-Tucker theory requires to consider the state constraints in the space of continuous functions. The continuity of solutions to (1)-(6) is shown by using maximum parabolic regularity results. After stating optimality conditions, we will turn to the numerical treatment of this optimization problem by means of a Moreau-Yosida type regularizaton of the state constraints. The feasibility of this approach is afterwards demonstrated by the example of hardening a gear rack used in the automotive industry.